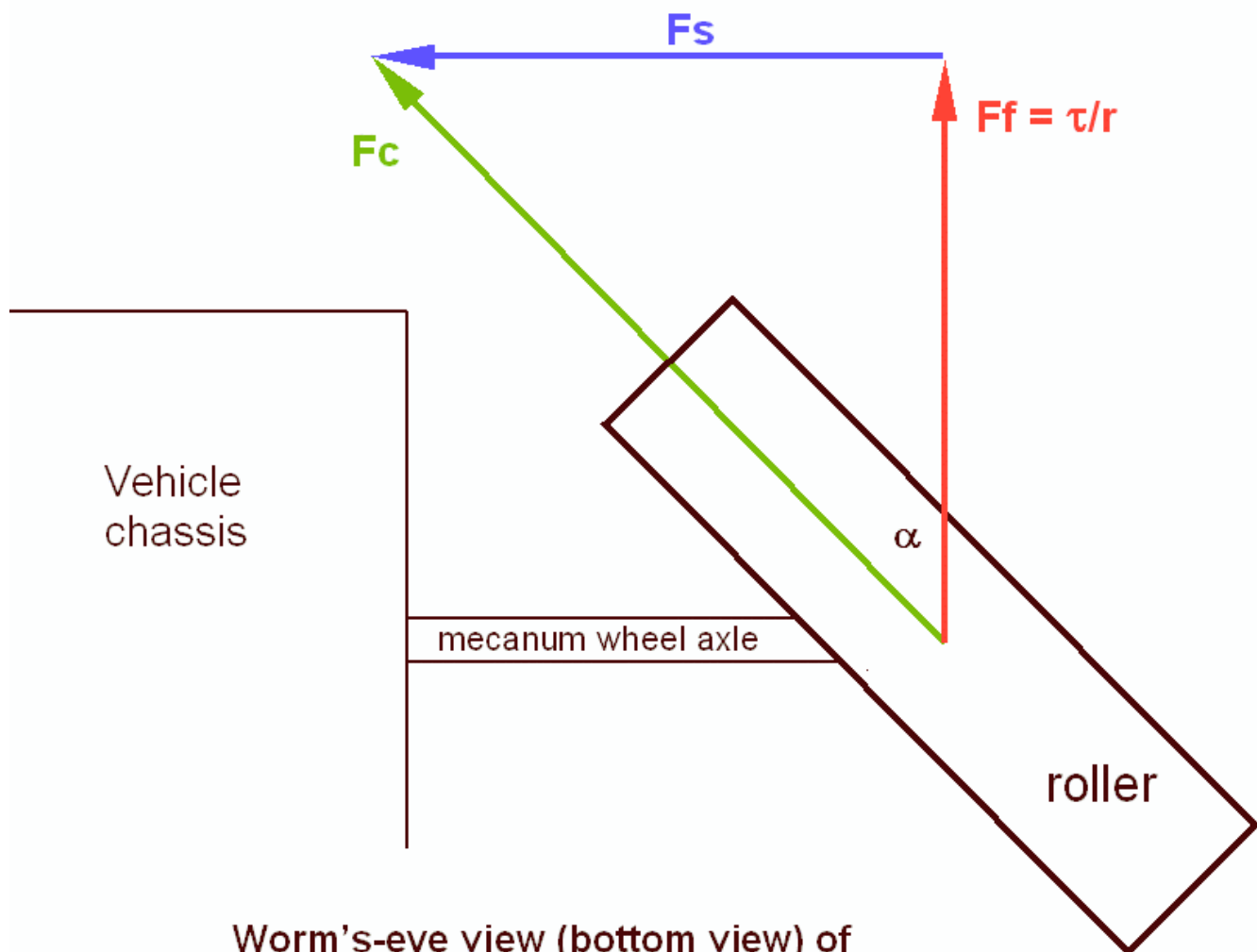


This paper explains why a mecanum-wheeled vehicle has less traction (and thus less “pushing force”) than a standard-wheel vehicle, even if both vehicles have the same motors, drivetrain, weight, and tread material.

Figure 1 below shows a “worm’s-eye” view of the roller of the front port-side mecanum wheel of a vehicle with four mecanum wheels. The vectors are drawn for the wheel being driven in the “forward” direction.



Worm’s-eye view (bottom view) of front port-side mecanum wheel *roller* in contact with floor (wheel itself not shown)

The green vector F_c is the reaction force of the floor on the bottom of the mecamum roller which is in contact with the floor. Assuming no friction in the roller bearings, this force *must be aligned along the roller axis* (assuming the roller is not accelerating).

F_c has two components, F_s and F_f .

F_s is counterbalanced by an equal but opposite force from the wheel on the other side of the vehicle (when that wheel is being driven with the same torque). This would be the case when the vehicle is to be driven straight forward.

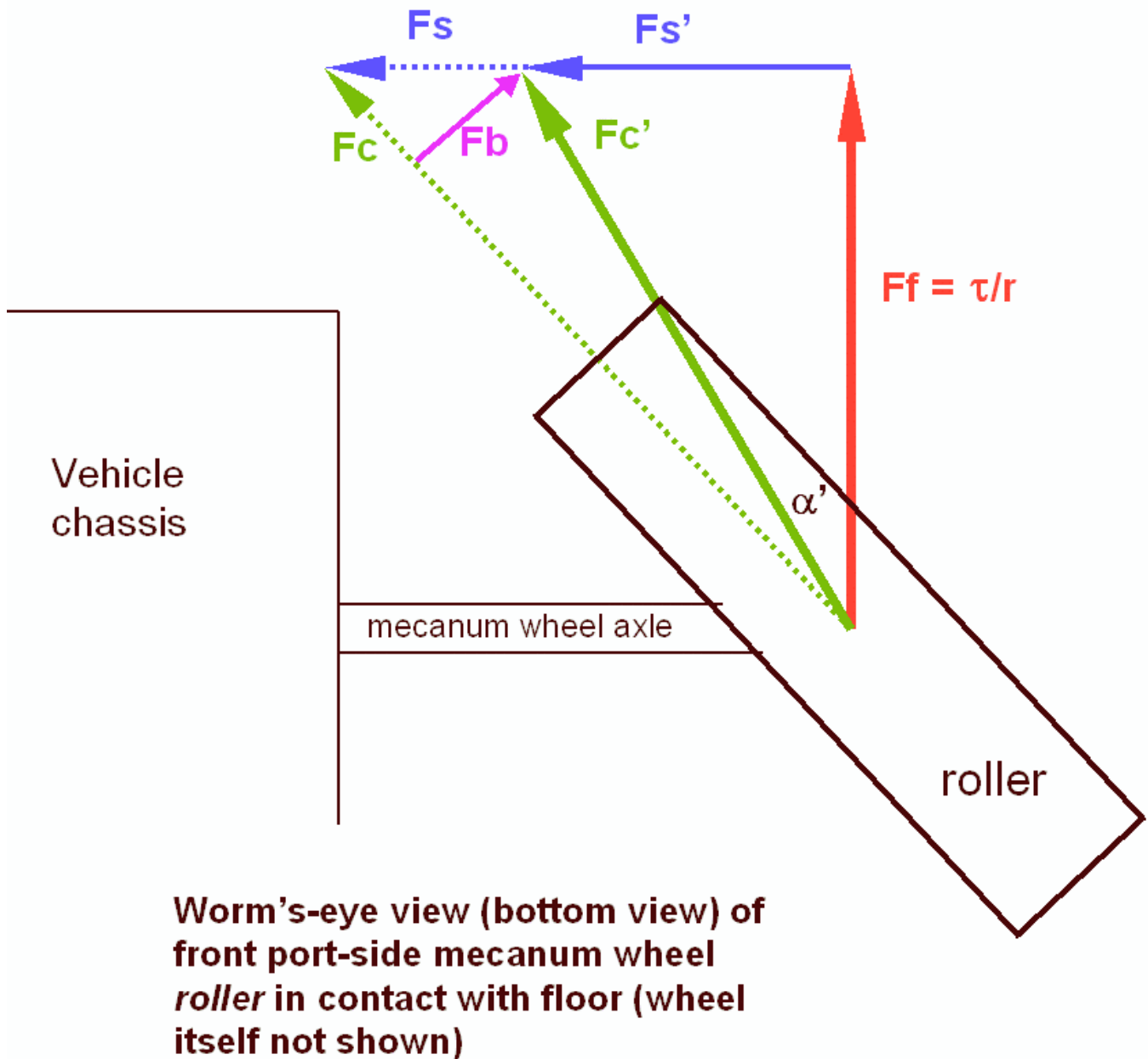
F_f is the forward component and is in the plane of the mecamum wheel. Assuming the wheel is not accelerating (constant or zero speed of the vehicle), *the net torque on the wheel must be zero*. Therefore F_f must be equal to τ/r , where " τ " is the driving torque applied to the mecamum wheel, and " r " is the radius of the mecamum wheel. The torque $r \cdot F_f$ counterbalances the driving torque τ , for a *net torque of zero on the wheel*. This in turn implies that F_c must equal $F_f/\cos(\alpha)$.

Note that the forward force F_f provided by this mecamum wheel *is the same as the forward force that would be produced by a "standard" wheel of the same diameter being driven with the same torque*; but in the case of the mecamum wheel the reaction force of the floor on the wheel (roller) is greater by a factor $1/\cos(\alpha)$. *It is this greater reaction force which causes the mecamum wheel to break friction with the floor and slip at lower forward-force levels than a standard wheel*. This explains why a mecamum vehicle has less traction than a standard-wheel vehicle, even if they both use the same wheel material.

Now consider the case where the vehicle is strafing toward starboard (to the left in Figure 1 since it is a bottom view).

When strafing, the rear port-side wheel is driven with the same magnitude of torque as the wheel shown in Figure 1, but in the "backwards" direction. F_f in Figure 1 is counterbalanced by an equal but opposite force from the back wheel of the vehicle. F_s will be in the same direction for the front and rear wheels and, for a 45 degree roller angle, it will have the exact same magnitude as F_f . Therefore, assuming no roller bearing friction, the "pushing force" (and speed) of the vehicle is the same in the fore/aft and sideways directions.

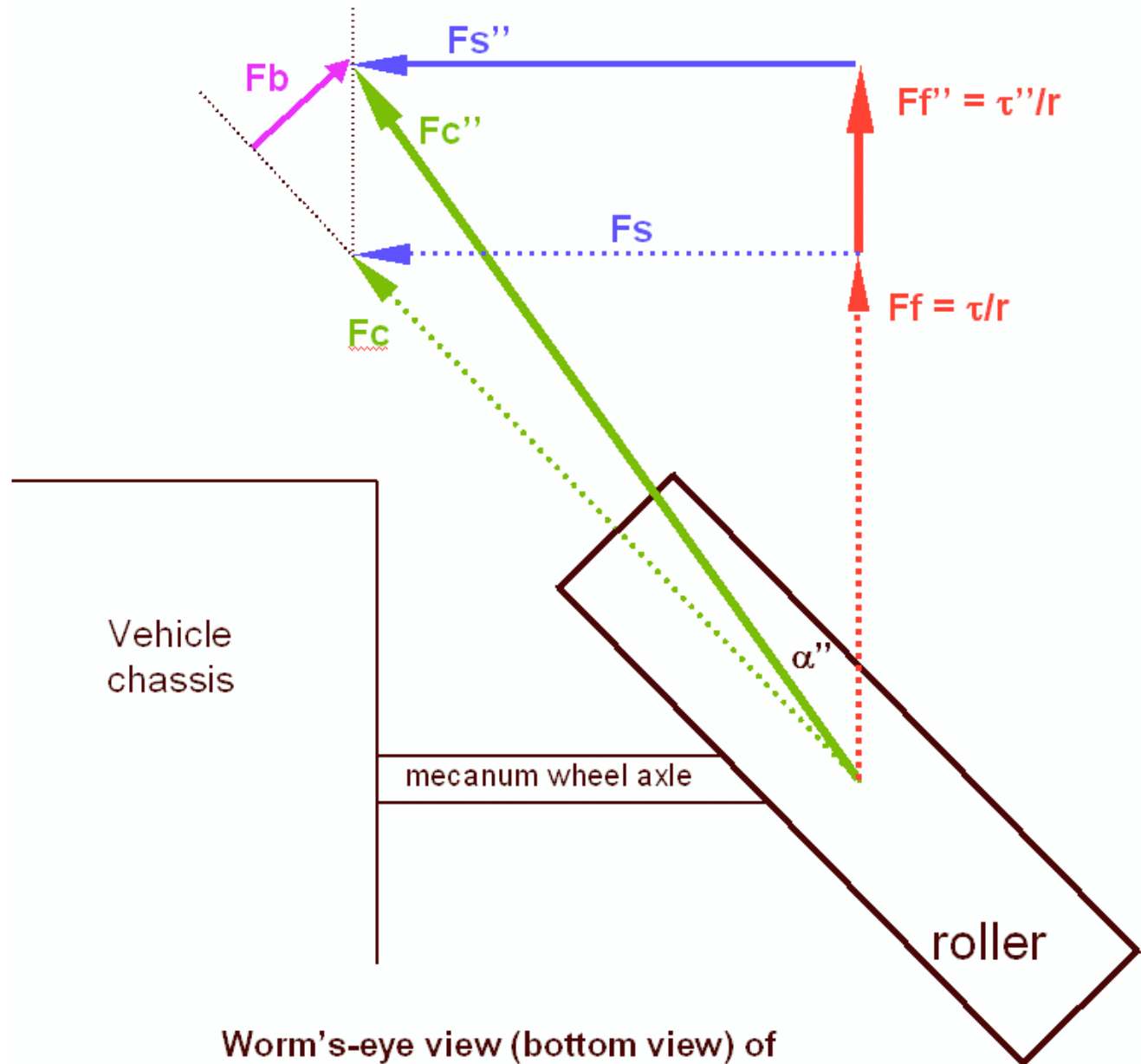
Note that the green vector F_c acting along the axis of the roller will slide the roller along its axle until all the free play has been taken up and the roller encounters something to prevent further axial movement. If this "something" is, for example, a ball bearing, friction will be minimized. Otherwise this contact, especially if it is rubber-on-metal, will create friction. This friction affects the analysis, as shown in Figures 2 and 3 and ensuing discussion on the following pages:



The vectors shown in dotted lines are there for reference only. The forward-force vector F_f remains unchanged; it must still equal τ/r . A new vector F_b has been introduced due to the roller bearing friction. The introduction of the F_b vector reduces the angle and magnitude of the F_c vector; it is now $F_{c'}$. The reduced magnitude of $F_{c'}$ means that greater forward force F_f can be applied (by increasing the driving torque) before the roller breaks friction with the ground. This gives the mecanum wheel greater traction (in the fore/aft direction). Roller bearing friction improves traction in the fore/aft direction.

In the sideways direction, the F_s magnitude has been reduced to $F_{s'}$ by the introduction of roller bearing friction F_b . For the same motor-driving torque as the friction-free case, the available sideways pushing

force has been reduced (from F_s to F_s'). This means that the motor torque must be increased from $\tau = F_f \cdot r$ to $\tau' = F_f' \cdot r$ (see Figure 3 below) to obtain the same sideways driving force F_s' as the friction-free case F_s . The necessary increase in motor torque to get the same sideways force as the friction-free case also increases the reaction force to F_c' so that it is greater than the friction-free reaction force F_c . Roller bearing friction reduces traction and available force in the sideways direction.



Worm's-eye view (bottom view) of front port-side mecanum wheel roller in contact with floor (wheel itself not shown)

On a final note, please note that the vector force analysis for an "omni" wheel (a wheel with rollers mounted along its circumference with axles in the plane of the wheel and tangent to the wheel's circumference) is different. Omni wheels, unlike mecanum wheels, are mounted at a 45 degree angle to the fore/aft axis of the robot.